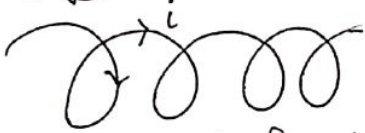


Calculation of Self-inductance

i) Long Solenoid :- (air core)



Magnetic induction at a point inside long solenoid

$$= B = \left(\frac{\mu_0 N I}{l} \right)$$

$N \rightarrow$ total number of turns

$l \rightarrow$ length of solenoid

$A \rightarrow$ area of cross-section.

Flux linked with each turn

$$= \phi_1 = B \cdot A = \left(\frac{\mu_0 N I}{l} \right) A$$

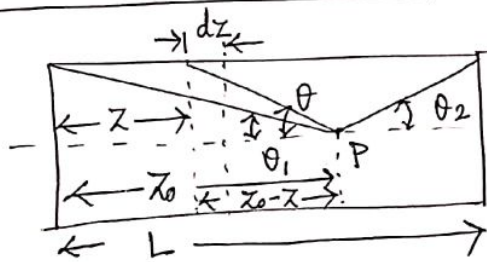
\therefore flux linked with 'N' turns

$$= \phi = N \phi_1 = \left(\frac{\mu_0 N^2 I}{l} \right) \cdot A$$

$$\therefore \text{Self inductance} = L = \frac{\phi}{I} = \frac{\mu_0 N^2 A}{l} \quad \left(\begin{array}{l} \text{solenoid} \\ \text{Toroid} \end{array} \right)$$

Self inductance of solenoid / Toroidal coil of 'N' number of turns of mean length 'l'.

If solenoid is not very long :-



$$\sin \theta = \frac{a}{\sqrt{a^2 + (z_0 - z)^2}}$$

$$\tan \theta = \frac{a}{(z_0 - z)}$$

$$\text{or } \frac{-a}{(z - z_0)} = \tan \theta$$

$$\text{or } (z - z_0) = -a \cot \theta$$

$$dz = (a \operatorname{cosec}^2 \theta) d\theta$$

$$= \frac{a}{\sin^2 \theta} d\theta$$

Magnetic induction at 'P' due to 'dz' this element is given by

~~$$dB = \left(\frac{N}{L} \right) dz \cdot \frac{\mu_0 I a^2}{2 [a^2 + (z_0 - z)^2]^{3/2}}$$~~

$$dB = \left(\frac{N}{L} \right) dz \cdot \frac{\mu_0 I a^2}{2 [a^2 + (z_0 - z)^2]^{3/2}}$$

$$= \left(\frac{N}{L} \right) \frac{\mu_0 I \cdot a^2}{2} \times \frac{a}{[a^2 + (z_0 - z)^2]^{3/2}} \times \frac{a d\theta}{\sqrt{a^2 + (z_0 - z)^2}}$$

$$= \left(\frac{N}{L} \right) \cdot \frac{\mu_0 I}{2} \cdot (\sin^2 \theta) \cdot (\sin \theta) \cdot \frac{a d\theta}{(\sin^2 \theta)}$$

$$= \frac{\mu_0 N I}{2L} \sin \theta d\theta$$

$$\therefore B = \int_{\theta_1}^{\theta_2} \frac{\mu_0 N I}{2L} \sin \theta d\theta = \frac{\mu_0 N I}{2L} (\cos \theta_1 + \cos \theta_2)$$

$$= \frac{\mu_0 N I}{2L} \left[\frac{z_0}{\sqrt{z_0^2 + a^2}} + \frac{(L - z_0)}{\sqrt{a^2 + (L - z_0)^2}} \right]$$

For small length dx_0 ,

Number of turns is $\left(\frac{N}{L}\right) \cdot dx_0$

\therefore Flux linking these turns

$$d\phi = \frac{B(\pi a^2)(N)}{L} dx_0$$

\therefore Total flux linking 'N' turns is

$$\Phi = \int_{z_0=0}^L \frac{B(\pi a^2)N}{L} \cdot dx_0$$

$$= \int_{z_0=0}^L \left(\frac{\mu_0 NI}{2L} \right) \left[\frac{z_0}{\sqrt{z_0^2 + a^2}} + \frac{(L-z_0)}{\sqrt{a^2 + (L-z_0)^2}} \right] (\pi a^2) \times \frac{N}{L} \cdot dz_0$$

$$= (\pi a^2) \frac{\mu_0 N^2 I}{2L^2} \left[\sqrt{a^2 + z_0^2} - \sqrt{a^2 + (L-z_0)^2} \right]_{z_0=0}^L$$

$$= (\mu_0 \pi a^2) \frac{IN^2}{2L^2} \left[\sqrt{a^2 + L^2} - a - a + \sqrt{a^2 + L^2} \right]$$

$$= \frac{\mu_0 N^2 (\pi a^2)}{L^2} \left[\sqrt{a^2 + L^2} - a \right] I$$

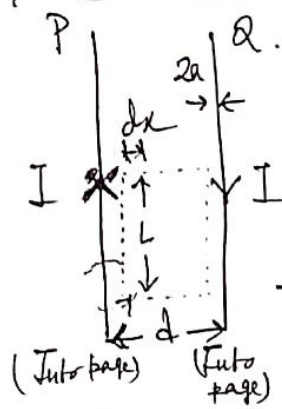
$$\text{(Self inductance)} L = \frac{\mu_0 N^2 (\pi a^2)}{L^2} \left[\sqrt{a^2 + L^2} - a \right]$$

if, $L \gg a$, then, $\sqrt{a^2 + L^2} \approx L$

$$\therefore L = \frac{(\mu_0 N^2) (\pi a^2)}{L^2} \times L \approx \frac{\mu_0 N^2 A}{L}$$

variation of magnetic flux over cross-sectional area being neglected

Self inductance of two long parallel wires:-



Let 'P' and Q be two long parallel wires separated by distance 'd'

Two wires carry same current 'I' in opposite direction

These two wires construct an open-air transmission line.

Radius 'a' of each wire, $a \ll d$.

\therefore Flux inside wires themselves can be neglected

The flux is concentrated betⁿ region betⁿ two wires.

Consider rectangular area

length $\rightarrow L$, width dx , at 'x' distance from wire

\therefore Flux through rectangle

$$d\phi = B \cdot L \cdot dx$$

$$\therefore \phi = \int_{x=a}^{d-a} \frac{\mu_0 I}{2\pi} \left(\frac{1}{x} + \frac{1}{(d-x)} \right) L \cdot dx$$

$$= \frac{\mu_0 I L}{2\pi} \left[\ln(x) - \ln(d-x) \right]_{x=a}^{d-a}$$

$$= \frac{\mu_0 I L}{2\pi} \left[\ln \left(\frac{x}{d-x} \right) \right]_{x=a}^{d-a}$$

$$= \frac{\mu_0 I L}{2\pi} \left[\ln \left(\frac{d-a}{a} \right) - \ln \left(\frac{a}{d-a} \right) \right]$$

$$= \frac{\mu_0 I L}{\pi} \ln \left(\frac{d-a}{a} \right) = LI$$

Since, $d \gg a$, self-inductance per unit length

$$\boxed{L/l = \frac{\mu_0}{\pi} \ln(d/a)}$$

if wires are very close together, $(d-a) \approx a$.

$\therefore L \approx 0$. This is the principle of

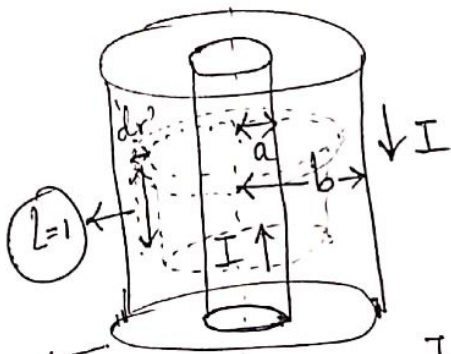
NON-INDUCTIVE WINDING,

used to construct resistance coils. ~~Insulated~~

Insulated coil is doubled on itself before it is wound on form.

~~both wires~~
~~field~~
~~lines~~
flux lines
adds up
in antiparalle
currents
but if
cancellation
of
parallel
currents

Coaxial. cylinders :-



Two Co-axial cylinders of radii 'a' and 'b' where $a < b$, carry same current 'I' in opposite direction.

They thus form Co-axial Cable.

Outside two cylinder mag. field is zero.

If we consider a circle of radius 'r' $r > b$, for concentric cable,

Total Current $I - I = 0$

if $a < r < b$,

$B = \left(\frac{\mu_0 I}{2\pi r} \right)$ (and $b \gg a$)

Flux = $\int_{r=a}^b \left(\frac{\mu_0 I}{2\pi r} \right) (dr \cdot 1)$ ← Imagine two Co-axial cylinders of radii r and $r+dr$, of unit length ($l=1$)

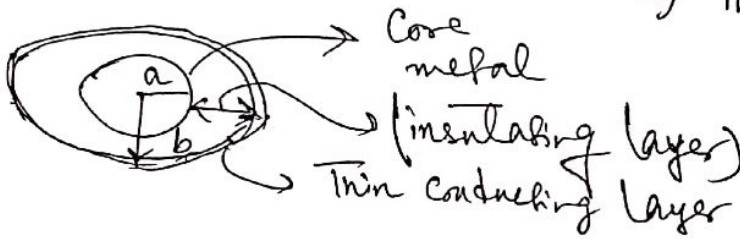
= $\frac{\mu_0 I}{2\pi} \ln(b/a)$

∴ 'L' (Inductance) per unit length = $\frac{\mu_0}{2\pi} \ln(b/a)$

Here, we have neglected flux inside materials of two cylinders.

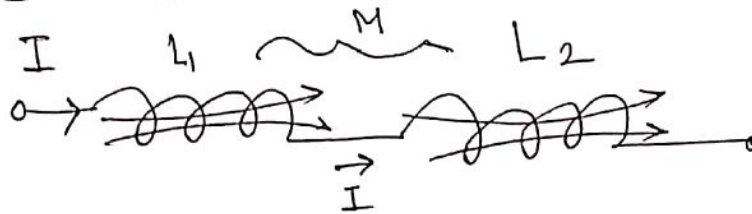
Justified, when 1) $(b \gg a)$

2) Thickness of outer cylinder ~~is~~ is very thin.



(construction of Co-axial Cable)

Inductances in Series



E.m.f in coil 1

$$E_{11} = -L_1 \left(\frac{dI}{dt} \right)$$

Emf induced in coil 2

due to current I in coil 1

$$E_{21} = -M \left(\frac{dI}{dt} \right) \quad , \quad M \rightarrow \text{Mutual inductance between coils}$$

\therefore Emf induced in coil 2

$$E_{22} = -L_2 \left(\frac{dI}{dt} \right)$$

Emf induced in coil 1.

due to current I in coil 2

$$E_{12} = -M \left(\frac{dI}{dt} \right)$$

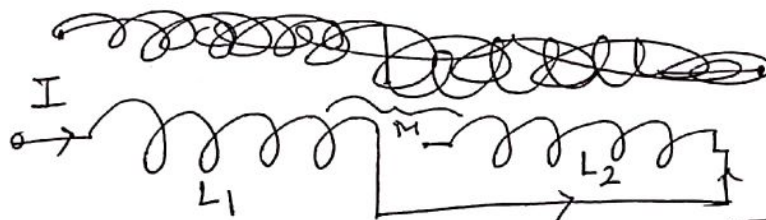
$$\text{Net emf} = E = E_{11} + E_{22} + E_{12} + E_{21}$$

$$= -(L_1 + L_2 + 2M) \left(\frac{dI}{dt} \right)$$

$$\therefore E = -L_{eq} \left(\frac{dI}{dt} \right)$$

$$\therefore \boxed{L_{eq} = L_1 + L_2 + 2M}$$

For anti-series connection



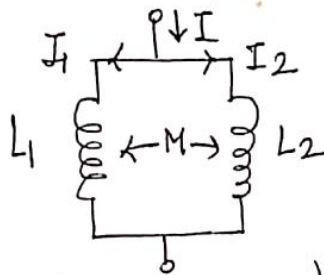
$$E = (E_{11} + E_{12} - E_{22} - E_{21})$$

$$\therefore \boxed{L_{eq} = L_1 + L_2 - 2M}$$

if $M=0$,

$$\boxed{L_{eq} = L_1 + L_2} \quad \checkmark$$

Parallel Inductances Parallel



$$\mathcal{E}_1 = -L_1 \left(\frac{dI_1}{dt} \right) - M \left(\frac{dI_2}{dt} \right)$$

$$\mathcal{E}_2 = -L_2 \left(\frac{dI_2}{dt} \right) - M \left(\frac{dI_1}{dt} \right)$$

As coils are parallel $\mathcal{E}_1 = \mathcal{E}_2 = \mathcal{E}$

$$\therefore \left. \begin{aligned} +L_1 \left(\frac{dI_1}{dt} \right) + M \left(\frac{dI_2}{dt} \right) &= -\mathcal{E} \\ M \left(\frac{dI_1}{dt} \right) + L_2 \left(\frac{dI_2}{dt} \right) &= -\mathcal{E} \end{aligned} \right\}$$

$$\therefore \left(\frac{dI_1}{dt} \right) = \frac{\begin{vmatrix} -\mathcal{E} & M \\ -\mathcal{E} & L_2 \end{vmatrix}}{\begin{vmatrix} L_1 & M \\ M & L_2 \end{vmatrix}} = \frac{-\mathcal{E}(L_2 - M)}{(L_1 L_2 - M^2)}$$

$$\left(\frac{dI_2}{dt} \right) = \frac{\begin{vmatrix} L_1 & -\mathcal{E} \\ M & -\mathcal{E} \end{vmatrix}}{\begin{vmatrix} L_1 & M \\ M & L_2 \end{vmatrix}} = \frac{-\mathcal{E}(L_1 - M)}{(L_1 L_2 - M^2)}$$

$$\text{Now, } \left(\frac{dI}{dt} \right) = \left(\frac{dI_1}{dt} \right) + \left(\frac{dI_2}{dt} \right) = \frac{-\mathcal{E}(L_1 + L_2 - 2M)}{(L_1 L_2 - M^2)}$$

$$\text{As, } \mathcal{E} = -L_{\text{eq}} \left(\frac{dI}{dt} \right) = -L_{\text{eq}} \times \left\{ \frac{-\mathcal{E}(L_1 + L_2 - 2M)}{(L_1 L_2 - M^2)} \right\}$$

$$\therefore \boxed{L_{\text{eq}} = \frac{L_1 L_2 - M^2}{(L_1 + L_2 - 2M)}} \checkmark$$

If Mutual inductance opposes self inductance

$$\boxed{L_{\text{eq}} = \frac{L_1 L_2 - M^2}{(L_1 + L_2 + 2M)}} \checkmark$$

$$\text{If } M=0, \quad \boxed{L_{\text{eq}} = \frac{L_1 L_2}{L_1 + L_2}} \checkmark$$

Coefficient of coupling :- Mutual flux betⁿ two coils may be less, at best equal to self fluxes of two coils.

$$\therefore \Phi_{12} \leq \Phi_{22} \text{ and } \Phi_{21} \leq \Phi_{11}$$

$$\therefore \Phi_{12} = K_1 \Phi_{22} \text{ and } \Phi_{21} = K_2 \Phi_{11}$$

$$\begin{aligned} \therefore M I_2 = \Phi_{12} = K_1 \Phi_{22} = K_1 L_2 I_2 &\Rightarrow M = K_1 L_2 \\ \text{and } M I_1 = \Phi_{21} = K_2 \Phi_{11} = K_2 L_1 I_1 &\Rightarrow M = K_2 L_1 \end{aligned} \left\{ \begin{aligned} \therefore M^2 &= K_1 K_2 L_1 L_2 \\ \therefore M &= K \sqrt{L_1 L_2} \end{aligned} \right.$$

When, $0 \leq K \leq 1$, 'K' \rightarrow "coefficient of coupling" of loops.

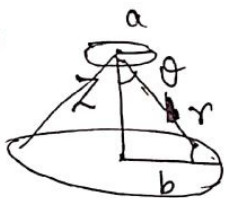
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 2) A small loop of wire (radius a) lies a distance ' z ' above the center of a large loop (radius b). The planes of two loops are parallel, and $\perp r$ to the common axis.

a) Suppose current ' I ' flows in the big loop. Find the flux through the little loop. (The little loop is so small that you may consider the field of the big loop is essentially constant).

b) Suppose current ' I ' flows in the little loop. Find the flux through the big loop. (The little loop is so small that you may treat it as a magnetic dipole).

c) Find the mutual inductance and confirm $M_{12} = M_{21}$.

Proof:



\Rightarrow flux through little loop

$$\Phi_{\text{little}} = \left[\frac{\mu_0 I b^2}{2(b^2 + z^2)^{3/2}} \right] (\pi a^2)$$

b) Flux through big loop

$$\Phi_{\text{big}} = \int B \cdot d\mathbf{s} =$$

\hookrightarrow (Field along axis) of small loop.

$$B = \frac{\mu_0}{4\pi} \frac{m}{r^3} (2\cos\theta \hat{r} + \sin\theta \hat{\theta})$$

where $m =$ magnetic moment $= (I \pi a^2)$ of little loop

\hookrightarrow mag. field due to a ~~small~~ small current loop, which is equivalent

to magnetic dipole.

$$\therefore \Phi_{\text{big}} = \frac{\mu_0 (I \pi a^2)}{4\pi r^3} \int \int (2\cos\theta) \cdot (r^2 \sin\theta) d\theta d\phi$$

$$= \frac{\mu_0 I a^2}{2r} \times 2\pi \times \frac{1}{2} \int_0^\theta \sin(2\theta) d\theta$$

$$= \frac{\mu_0 I a^2}{r} \times \frac{\pi}{2} \left[-\frac{\cos(2\theta)}{2} \right]_0^\theta$$

$$= \frac{\mu_0 I a^2}{r} \cdot \frac{\pi}{4} \times [1 - \cos(2\theta)] = \frac{(\mu_0 I a^2) \pi}{4r} [2 \sin^2\theta]$$

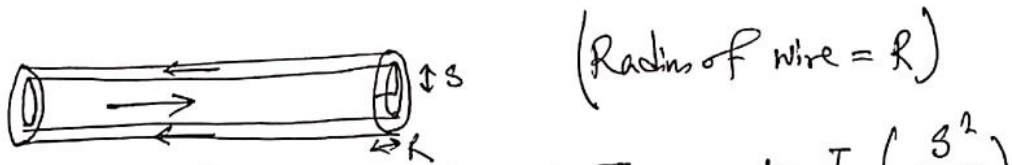
$$\therefore M_{12} = M_{21} = \frac{\mu_0 \pi a^2 b^2}{2(b^2 + z^2)^{3/2}}$$

$$= \frac{(\mu_0 I a^2) \pi}{2} \times \frac{1}{r} \times \left(\frac{b}{r}\right)^2 = \frac{(\mu_0 I a^2) \pi}{2} \times \frac{b^2}{(z^2 + b^2)^{3/2}}$$

\leftarrow Integrating over "spherical cap" bounded by big loop and centered at little loop

Q7.28 A long cable carries current in one direction uniformly distributed over its (circular) cross-section. The current returns along the surface (there is very thin insulating sheath separating currents). Find self inductance per unit length.

Solⁿ:-



$$\oint \vec{B} \cdot d\vec{l} = B(2\pi s) = \mu_0 I_{enc} = \mu_0 I \left(\frac{s^2}{R^2} \right)$$

$$\therefore B = \mu_0 I \left(\frac{s^2}{R^2} \right) \times \left(\frac{1}{2\pi s} \right)$$

$$= \frac{\mu_0 I s}{2\pi R^2}$$

$$\therefore W = \frac{1}{2\mu_0} \int_0^R B^2 dV$$

$$= \frac{1}{2\mu_0} \int_0^R \frac{\mu_0^2 I^2 s^2}{4\pi^2 R^4} \cdot (2\pi s) l \cdot ds$$

Cylindrical volume element

$$= \frac{\mu_0 I^2}{8\pi R^4} \times (2\pi l) \int_0^R \left[\frac{s^4}{4} \right] ds$$

$$= \frac{\mu_0 I^2}{16\pi} \times L \times \left(\frac{R^4}{R^4} \right) = \frac{1}{2} L I^2 \quad \left(\begin{array}{l} \text{Energy stored in} \\ \text{coil} \end{array} \right)$$

$$\therefore \boxed{L = \frac{\mu_0 L}{8\pi}} \Rightarrow \text{Self inductance per unit length} = \frac{L}{l} = \frac{\mu_0}{8\pi} \text{ sol}^n$$