

# Introduction to Maxwell's eqns. Charge conservation

①

## Displacement Current and resurrection by $\epsilon_0$ Eqn of Continuity

### Electrodynamics Before Maxwell

i)  $\vec{\nabla} \cdot \vec{E} = \rho / \epsilon_0$  (Gauss's law)

ii)  $\vec{\nabla} \cdot \vec{B} = 0$

iii)  $\vec{\nabla} \times \vec{E} = - \frac{\partial \vec{B}}{\partial t}$  (Faraday's law)

iv)  $\vec{\nabla} \times \vec{B} = \mu_0 \vec{J}$  (Ampere's law)

Inconsistency in these formulas.

$$\vec{\nabla} \cdot (\vec{\nabla} \times \vec{E}) = \vec{\nabla} \cdot \left( - \frac{\partial \vec{B}}{\partial t} \right) = - \frac{\partial}{\partial t} (\vec{\nabla} \cdot \vec{B}) = 0 \quad \underline{\text{all time}}$$

But,  $\vec{\nabla} \cdot (\vec{\nabla} \times \vec{B}) = \mu_0 (\vec{\nabla} \cdot \vec{J})$

L.H.S = 0, But right hand side  $\neq 0$  in general

For steady currents, the divergence of  $\vec{J}$  is zero.

But beyond Magnetostatics. i.e. Varying current case  
Ampere's law cannot be right

In. Integral form Ampere's law reads

$$\oint \vec{B} \cdot d\vec{l} = \mu_0 I_{enc}$$

### Eqn of Continuity

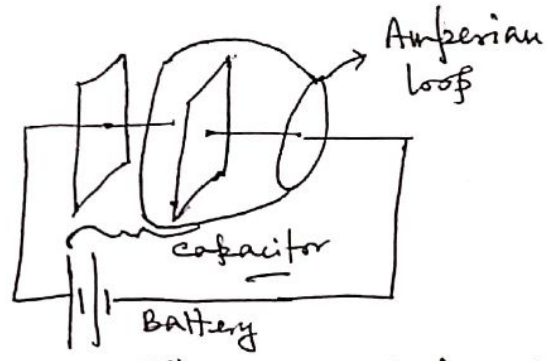
Volume  $v$  bounded by surface  $s$ .

$\frac{dq}{dt} = i = \oint_s \vec{J} \cdot d\vec{s} \dots$  ①  $\vec{J} \rightarrow$  volume current density.

$\therefore i = \oint_s \vec{J} \cdot d\vec{s} = - \frac{dq}{dt} = - \int_v \left( \frac{\partial \rho}{\partial t} \right) dv$  | Current is rate of decrease of charge per unit time as total charge is conserved.

$\therefore \oint_s \vec{J} \cdot d\vec{s} + \int_v \left( \frac{\partial \rho}{\partial t} \right) dv = 0$

$\therefore \int_v (\vec{\nabla} \cdot \vec{J} + \frac{\partial \rho}{\partial t}) dv = 0 \Rightarrow \boxed{\vec{\nabla} \cdot \vec{J} + \frac{\partial \rho}{\partial t} = 0}$   
 $\hookrightarrow$  for arbitrary volume  $dv \neq 0$ .



we want to apply Ampere's law. to shown loop.

How to find  $I_{enc}$ ?

It is the total current passing through the loop, more precisely current piercing a surface that has the loop for its boundary. Here simplest surface lies in the plane of the loop — the wire punctures this surface, so  $I_{enc} = I$ .

But what if I draw the balloon shaped surface? No current passes through this surface.

$\therefore I_{enc} = 0$

We never had this problem in magnetostatics as the conflict arises only when charge is piling up somewhere. (here the capacitor plates).

~~For nonsteady currents~~  
Maxwell's sol<sup>n</sup> to problem

Applying eqn of continuity

$$\nabla \cdot \vec{J} = -\left(\frac{\partial \rho}{\partial t}\right) = -\frac{\partial}{\partial t} (\epsilon_0 \nabla \cdot \vec{E}) = -\nabla \cdot \left(\epsilon_0 \frac{\partial \vec{E}}{\partial t}\right)$$

$$\therefore \nabla \times \vec{B} = \mu_0 \vec{J} + \mu_0 \epsilon_0 \frac{\partial \vec{E}}{\partial t}$$

Gauss's law  
 $\rho = \epsilon_0 \nabla \cdot \vec{E}$

(So combining  $\epsilon_0 \frac{\partial \vec{E}}{\partial t}$  with  $\vec{J}$  in Ampere's law would be right to kill the extra divergence)

Such modification changes nothing as far magnetostatics is concerned.

When 'E' is constant, we still have  $\nabla \times \vec{B} = \mu_0 \vec{J}$ .

Maxwell's term is hard to detect in ordinary electromagnetic experiments, where it must compete for recognition with 'J'. Thus Faraday and others never discovered it in laboratory.

From  $\vec{\nabla} \times \vec{B} = \mu_0 \vec{J} + \mu_0 \epsilon_0 \left( \frac{\partial \vec{E}}{\partial t} \right)$

The Maxwell's term demands, like Faradays law:-  
change in magnetic field induces electric field.

$\Rightarrow$  (changing Electric field induces a magnetic field)

Maxwell called his extra term Displacement Current

$$J_d \equiv \epsilon_0 \left( \frac{\partial E}{\partial t} \right)$$

Now to resolve the paradox of Capacitor charging.  
If the Capacitor plates are very close together

$$E = \frac{V}{\epsilon_0} = \frac{Q}{\epsilon_0 A} \quad \left| \begin{array}{l} Q \rightarrow \text{charge on plate} \\ A \rightarrow \text{area} \end{array} \right.$$

$$\therefore \left( \frac{\partial E}{\partial t} \right) = \frac{1}{\epsilon_0 A} \left( \frac{dQ}{dt} \right) = \frac{1}{\epsilon_0 A} \cdot I$$

$$\therefore \oint \vec{B} \cdot d\vec{l} = \mu_0 I_{enc} + \mu_0 \epsilon_0 \int \left( \frac{\partial E}{\partial t} \right) \cdot d\vec{a}$$

If we choose a flat surface

then  $E = 0$  and  $I_{enc} = I \rightarrow$  (comes from genuine current)

If we choose a Balloon-shaped surface,

then,  $I_{enc} = 0$ , but  $\int \left( \frac{\partial \vec{E}}{\partial t} \right) \cdot d\vec{a} = I / \epsilon_0$

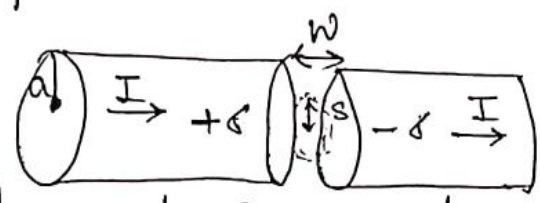
(comes from Displacement Current)

$$\begin{aligned} & \int_S \left( \frac{\partial \vec{E}}{\partial t} \right) \cdot d\vec{a} \\ &= \frac{d}{dt} \int_S (\vec{E} \cdot d\vec{a}) \\ &= \frac{d}{dt} \int_V (\vec{\nabla} \cdot \vec{E}) dV \\ &= \frac{d}{dt} \int_V \frac{\rho}{\epsilon_0} dV \\ &= \frac{1}{\epsilon_0} \cdot \left( \frac{dQ}{dt} \right) = \frac{I}{\epsilon_0} \end{aligned}$$

Displacement current related problem

2) A fat wire of radius 'a', carries a constant current 'I', uniformly distributed over its cross-section. A narrow gap in the wire of width  $w \ll a$  forms a parallel plate capacitor. Find the magnetic field in the gap at a distance  $s < a$  from the axis. (1)

Sol<sup>n</sup>:



Displacement Current density  
 $= J_d = \epsilon_0 \left( \frac{\partial E}{\partial t} \right) = \frac{I}{A} = \frac{I}{\pi a^2} \hat{z}$

Drawing an "Amperian loop" at radius 's'

$$\oint \vec{B} \cdot d\vec{l} = B \cdot 2\pi s = \mu_0 I_{enc}$$

$$= \mu_0 \left( \frac{I}{\pi a^2} \right) (\pi s^2)$$

$$= \mu_0 I \frac{s^2}{a^2}$$

$$\therefore B = \frac{1}{2\pi s} \times \frac{\mu_0 I s^2}{a^2} = \frac{\mu_0 I s}{2\pi a^2} \hat{\phi}$$

2) A thin wire that connect to the centers of the plates (forming capacitor plates)

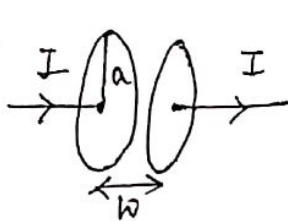
Again current 'I' is constant, radius of capacitor is 'a', separation of the plates  $w \ll a$ .

Assume the current flows out over the plates in such a way that the surface charge is uniform, at any given time, and zero at  $t=0$ .

- i) Find electric field bet<sup>n</sup> the plates as a function of 't'
- ii) Find the displacement current through a circle of radius 's' in the plane midway bet<sup>n</sup> the plates. Using this circle as your "Amperian loop", and the flat surface that spans it, find the magnetic field at a distance 's' from the axis.
- iii) Find displacement current through a cylindrical surface, which extends to the left through the plate and terminates outside the capacitor.

# Displacement Current related problem

Q2) Sol<sup>n</sup>



$w \ll a$   
 Surface current is uniform at 't'  
 Surface current = 0 at " $t=0$ "

i)  $E = \frac{\sigma(t)}{\epsilon_0} \hat{z}$  ,  $\sigma(t) = \frac{Q(t)}{\pi a^2} = \frac{I \cdot t}{\pi a^2}$

$\therefore$  Electric field between plates =  $\vec{E} = \frac{\sigma(t)}{\epsilon_0} \hat{z} = \frac{I t}{\epsilon_0 \pi a^2} (\hat{z})$

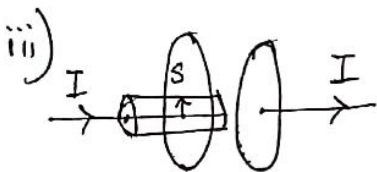
ii) Displacement current through circle

of radius 's' =  $I_{disc} = I_d \cdot \pi s^2$   
 $= \epsilon_0 \left( \frac{\partial E}{\partial t} \right) \cdot \pi s^2 = \epsilon_0 \frac{\partial}{\partial t} \left[ \frac{I t}{\epsilon_0 \pi a^2} \right] \cdot \pi s^2$   
 $= \epsilon_0 \cdot \frac{I}{\epsilon_0 \pi a^2} (\pi s^2)$   
 $= I (s^2/a^2)$

$\therefore \oint \vec{B} \cdot d\vec{l} = \mu_0 I_{disc}$

$\therefore (2\pi s) B = \mu_0 I (s^2/a^2)$

$\therefore B = \frac{\mu_0 I}{2\pi a^2} \times (s^2/a^2) = \left( \frac{\mu_0 I}{2\pi a^2} \right) s \hat{\phi}$  } Magnetic field at a distance 's' from the axis



A surface current flows radially outward over the left plate.

$I(s)$  be total current crossing a circle of radius 's'.

$\therefore$  charge density at time (t) is  
 $= \sigma(t) = \frac{[I - I(s)] t}{\pi s^2}$

Since ~~this is~~ we are told this is independent of 's',  $\sigma(t)$  is

$\therefore I - I(s) = \beta s^2$  ( $\beta$  is some constant)

But  $I(a) = 0$ ,  $\therefore \beta a^2 = I \therefore \beta = \frac{I}{a^2}$

$\therefore \beta = (I/a^2)$

$\therefore I(s) = I - \beta s^2 = I - \frac{I}{a^2} s^2 = I (1 - s^2/a^2)$

$\therefore B(2\pi s) = \mu_0 I_{enc} = \mu_0 [I - I(s)]$

$= (I - I + I s^2/a^2) \cdot \mu_0$

$\therefore B = \mu_0 I \frac{s^2}{a^2} \times \frac{1}{(2\pi s)} = \frac{\mu_0 I}{2\pi a^2} s \hat{\phi}$  ✓

Q3 If  $E(s, t) = \frac{\mu_0 I_0 \omega}{2\pi} \sin(\omega t) \cdot \ln(a/s) \hat{z}$ . (3)

a) Find displacement current  $J_D$

b) Integrate it to get total displacement current

$$I_D = \int \vec{J}_D \cdot d\vec{a}$$

c) Compare  $I_D$  and  $I$ , (what is the ratio?)

If outer cylinder were 2mm in diameter, how high would be the frequency have to be for ' $I_D$ ' to be 1% of  $I$ ?

Sol<sup>n</sup>:- a)  $J_D = \epsilon_0 \left( \frac{\partial E}{\partial t} \right)$   
 $= \epsilon_0 \frac{\mu_0 I_0 \omega^2}{2\pi} \cos(\omega t) \cdot \ln(a/s) \hat{z}$

b)  $I_D = \int_0^a \frac{\epsilon_0 \mu_0 I_0 \omega^2}{2\pi} \cos(\omega t) \ln(a/s) \cdot (2\pi s) ds$   
 $= \frac{\mu_0 \epsilon_0 \omega^2 I_0 \cos(\omega t)}{2\pi} \int_0^a [s \ln(a) - s \ln(s)] ds$   
 $= \mu_0 \epsilon_0 \omega^2 I_0 \cos(\omega t) \left\{ \left[ \ln(a) \right] \frac{a^2}{2} - \left[ \frac{s^2}{2} \ln(s) - \int_0^a \frac{1}{s} \frac{s^2}{2} ds \right] \right\}$   
 $= \mu_0 \epsilon_0 \omega^2 I_0 \cos(\omega t) \left\{ \frac{a^2}{2} \ln(a) - \frac{a^2}{2} \ln(a) + \frac{a^2}{4} \right\}$

c)  $I_D/I = \left( \mu_0 \epsilon_0 \omega^2 \right) \frac{a^2}{4}$ , where  $I = I_0 \cos(\omega t)$   
 $= \frac{1}{c^2} \times \frac{\omega^2 a^2}{4} = \left( \frac{\omega a}{2c} \right)^2$

$a \approx 2 \text{ mm} = 10^{-3} \text{ m}$

Now,  $I_D/I = \frac{1}{100} = \left( \frac{\omega a \times 10^{-3}}{2c} \right)^2$

$\Rightarrow \frac{1}{100} = 10^{-1} = \frac{\omega \times 10^{-3}}{2c}$

$\therefore \omega = \frac{10^{-1} \times 2c}{10^{-3}} = 10^2 \times 2 \times 3 \times 10^8 = 6 \times 10^{10} \text{ Hz}$   
 $\sim 10^4 \text{ MHz}$

$\therefore$  ' $\omega$ ' has to be in microwave region

i.e. far above radiowave region.